ET 438 b Digital Control and Data Acquisition
Department of Technology

# Lesson 12: Analog Signal Conditioning 

## Learning Objectives

After this presentation you will be able to:
> Design a voltage-to-current interface for a transducer and simulate its operation using commonly available software
> List the modes of operation of a Wheatstone bridge circuit
> Explain how Wheatstone bridge resistor values effect linearity and sensitivity
> Design a signal conditioning circuit for a Wheatstone bridge.

## Analog-to-Analog Conversion Signal Conditioning

Current-to-Voltage Converter
I-to-V Converter
Example: Find a value the value of $R$ that converts a 4 mA to 20 mA
current signal into a $1-5 \mathrm{~V}$ output Voltage.

$$
\begin{aligned}
& \mathrm{V}_{\mathrm{o}}=\mathrm{I}_{\mathrm{in}} \cdot \mathrm{R} \Rightarrow \mathrm{R}=\frac{\mathrm{V}_{\mathrm{o}}}{\mathrm{I}_{\text {in }}} \\
& \mathrm{V}_{\mathrm{o}}=1 \mathrm{~V} @ \mathrm{I}_{\text {in }}=4 \mathrm{~mA} \\
& \mathrm{R}=\frac{1 \mathrm{~V}}{4 \mathrm{~mA}}=250 \Omega
\end{aligned}
$$

Since $\mathrm{V}^{+}=\mathrm{V}^{-}$
Check output at 20 mA

$$
\mathrm{V}_{\mathrm{o}}=250 \Omega \cdot(20 \mathrm{~mA})=5 \mathrm{~V}
$$

$V_{o}=I_{\text {in }} \cdot R$

## Signal Conditioning

Voltage-to-Current Converter
V-to-I Converter (Transconductance Amps)


Ungrounded load
$\mathrm{V}^{+}=\mathrm{V}^{-}=\mathrm{V}_{\text {in }}$ and $\mathrm{I}_{\text {in }}=0$
So $I_{0}-I_{R}=0$ or $I_{0}=I_{R}$ $\mathrm{I}_{\mathrm{o}}=\mathrm{I}_{\mathrm{R}}=\frac{\mathrm{V}^{-}}{\mathrm{R}}$ but $\mathrm{V}^{-}=\mathrm{V}^{+}=\mathrm{V}_{\text {in }}$ $I_{o}=\frac{V_{\text {in }}}{R}$

Note: $R_{L}<R$ for practical circuit operation. OP AMP output voltage determines magnitude of $R_{L}$ for constant current

## Signal Conditioning Example

Convert a $0-5 \mathrm{~V}$ dc voltage signal to a $4-20 \mathrm{~mA}$ current signal using OP AMP circuits.


Determine the ratio of spans

$$
\mathrm{R} 6=\frac{\mathrm{V}_{\text {in }}}{\mathrm{I}_{0}}=\frac{\mathrm{V}_{\text {in(max) }}-\mathrm{V}_{\text {in(min) }}}{\mathrm{I}_{\mathrm{I}_{\text {max }}}-\mathrm{I}_{0 \text { min }}}=\frac{5 \mathrm{~V}-0 \mathrm{~V}}{20 \mathrm{~mA}-4 \mathrm{~mA}}=\frac{5 \mathrm{~V}}{16 \mathrm{~mA}}=312.5 \Omega
$$

## Signal Conditioning Example

Compute the value of Vbias to give the value of minimum output
current
$\mathrm{I}_{0 \text { min }}=4 \mathrm{~mA}$
$I_{0}=\frac{V_{\text {in }}}{R} \Rightarrow I_{0} \cdot R=V_{\text {in }}$
$\mathrm{V}_{\text {bias }}=\mathrm{I}_{0 \text { min }} \cdot \mathrm{R}$
$\mathrm{R}=312.5 \Omega$
$\mathrm{V}_{\text {bias }}=(4 \mathrm{~mA}) \cdot(312.5 \Omega)$
$\mathrm{V}_{\text {bias }}=1.25 \mathrm{~V}$

Check the output with
$V_{\text {in }}=5 \mathrm{~V}$
What in max value of $R_{L}$ ?
Assume $\mathrm{V}_{\text {sat }}=10.5 \mathrm{~V}$
$\mathrm{I}_{0}=\frac{\mathrm{V}_{\text {in }}}{\mathrm{R}}$
$\mathrm{V}_{\text {max }}=\mathrm{V}_{\text {in(max) }}+\mathrm{V}_{\text {bias }}$
$\mathrm{V}_{\text {max }}=5 \mathrm{~V}+1.25 \mathrm{~V}$
$\mathrm{I}_{0}=\frac{6.25 \mathrm{~V}}{312.5 \Omega}$
$\mathrm{I}_{0}=0.02 \mathrm{~A}=20 \mathrm{~mA}$
$\mathrm{R}_{\mathrm{L} \text { (max) }}=\frac{10.5 \mathrm{~V}-6.25 \mathrm{~V}}{0.02 \mathrm{~A}}=212.5 \Omega$
Assumes OP AMP has sufficient current output

## Circuit Simulation of Example: Dc Sweep

Output Current Vs Input Voltage

$\overline{\text { A }}$


## Instrumentation Amps with High Impedance Input

Two-stage circuit


$$
A_{v 1}=\left(\frac{E 2-E 1}{V 2-V 1}\right)=\frac{2 R 1}{R 2}+1
$$

$$
A_{\mathrm{v} 2}=\frac{V_{0}}{E 2-E 1}=\frac{R 4}{R 3}
$$



Overall circuit gain $\quad \mathrm{V}_{0}=\left(\frac{2 \mathrm{R} 1}{\mathrm{R} 2}+1\right) *\left(\frac{\mathrm{R} 4}{\mathrm{R} 3}\right) *(\mathrm{~V} 2-\mathrm{V} 1)$

## Signal Conditioning-Bridge Circuits

Dc bridges (Wheatstone bridges) Used to detect small resistance changes in sensors. Typically used with sensors that measure force, temperature, and pressure.


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## Bridge Use Methods

There are two operating modes for a dc bridge: balanced (null) and unbalanced
Null Mode - adjust $\mathrm{R}_{3}$ variable resistor until $\mathrm{l}_{\mathrm{ab}}=\mathrm{o}$. Need automatic nulling circuit for automatic operation.

Unbalanced Mode - insert sensor and null bridge for sensor measurement. When initial value of sensor changes measure difference in voltage. Bridge only balanced at one point

## Unbalanced Bridge Operation

Note the unbalanced bridge shown below. U1 and U2 provide high-Z input. Circuit gain provided by $\mathrm{U}_{3}$ using the following formula.


Find expression for bridge equation. in terms of the change in sensor resistance $R_{s}$.

## Unbalanced Bridge Analysis

Bridge Circuit


Normalize $\mathrm{V}_{\mathrm{ba}}$ by dividing by supply V .
Find common denominator

$$
\frac{V_{b}-V_{a}}{V_{d c}}=\left(\frac{R_{4}}{R_{3}+R_{4}}-\frac{R_{2}}{R_{s}+R_{2}}\right)=\frac{R_{4}\left(R_{s}+R_{2}\right)-R_{2}\left(R_{3}+R_{4}\right)}{\left(R_{3}+R_{4}\right)\left(R_{s}+R_{2}\right)}
$$

## Unbalanced Bridge Analysis

Bridge Analysis (Continued)
Expand terms and simplify

$$
\frac{V_{b}-V_{a}}{V_{d c}}=\frac{R_{4} R_{s}+R_{4} R_{2}-R_{2} R_{3}-B_{2} R_{4}}{\left(R_{3}+R_{4}\right)\left(R_{s}+R_{2}\right)}=\frac{R_{4} R_{s}-R_{2} R_{3}}{\left(R_{3}+R_{4}\right)\left(R_{s}+R_{2}\right)}
$$

From the previous balance equation

$$
\frac{R_{b a} R_{4}}{R_{3}}=R_{2}
$$

Substitute these equations into the above relationship

$$
\begin{gathered}
\frac{V_{b}-V_{a}}{V_{d c}}=\frac{R_{4} R_{s}-R_{b a l} R_{4}}{\left(R_{3}+R_{4}\right)\left(R_{s}+R_{b a l} R_{4} / R_{3}\right)} \\
\left(R_{3}+R_{4}\right)\left(R_{s}+R_{b a l} R_{4} / R_{3}\right)=R_{3} R_{s}+R_{4} R_{s}+R_{b a l} R_{4}+R_{b a l} R_{4}^{2} / R_{3}
\end{gathered}
$$

## Unbalanced Bridge Analysis

Bridge Analysis (Continued)
Combine the past two equations and clear $\mathrm{R}_{3}$ from the denominator.

$$
\frac{\mathrm{V}_{\mathrm{b}}-\mathrm{V}_{\mathrm{a}}}{\mathrm{~V}_{\mathrm{dc}}}=\frac{\mathrm{R}_{3} \mathrm{R}_{4}\left(\mathrm{R}_{\mathrm{s}}-\mathrm{R}_{\mathrm{bal}}\right)}{\mathrm{R}_{3}{ }^{2} \mathrm{R}_{\mathrm{s}}+\mathrm{R}_{3} \mathrm{R}_{4} \mathrm{R}_{\mathrm{s}}+\mathrm{R}_{3} \mathrm{R}_{4} \mathrm{R}_{\mathrm{bal}}+\mathrm{R}_{\mathrm{bal}} \mathrm{R}_{4}{ }^{2}}
$$

Now let $R_{4}=R_{3}$ and simplify further

$$
\begin{aligned}
& \frac{\mathrm{V}_{\mathrm{b}}-\mathrm{V}_{\mathrm{a}}}{\mathrm{~V}_{\mathrm{dc}}}=\frac{\mathrm{R}_{3}{ }^{2}\left(\mathrm{R}_{\mathrm{s}}-\mathrm{R}_{\mathrm{bal}}\right)}{\mathrm{R}_{3}{ }^{2}\left(2\left(\mathrm{R}_{\mathrm{s}}+\mathrm{R}_{\mathrm{bal}}\right)\right.}=\frac{\mathrm{R}_{3}{ }^{2}\left(\mathrm{R}_{\mathrm{s}}-\mathrm{R}_{\mathrm{bal}}\right)}{\mathrm{R}_{3}{ }^{2} \mathrm{R}_{\mathrm{s}}+\mathrm{R}_{3}{ }^{2} \mathrm{R}_{\mathrm{s}}+\mathrm{R}_{3}{ }^{2} \mathrm{R}_{\mathrm{bal}}+\mathrm{R}_{\mathrm{bal}} \mathrm{R}_{3}{ }^{2}} \\
& \frac{\mathrm{~V}_{\mathrm{b}}-\mathrm{V}_{\mathrm{a}}}{\mathrm{~V}_{\mathrm{dc}}}=\frac{\mathrm{R}_{3}{ }^{2}\left(\mathrm{R}_{\mathrm{s}}-\mathrm{R}_{\mathrm{bal}}\right)}{2 \mathrm{R}_{3}{ }^{2} \mathrm{R}_{\mathrm{s}}+2 \mathrm{R}_{3}{ }^{2} \mathrm{R}_{\mathrm{bal}}}=\frac{\mathrm{R}_{3}{ }^{2}\left(\mathrm{R}_{\mathrm{s}}-\mathrm{R}_{\mathrm{bal}}\right)}{\mathrm{R}_{3}{ }^{2}\left(2\left(\mathrm{R}_{\mathrm{s}}+\mathrm{R}_{\mathrm{bal}}\right)\right)} \\
& \frac{\mathrm{V}_{\mathrm{b}}-\mathrm{V}_{\mathrm{a}}}{\mathrm{~V}_{\mathrm{dc}}}=\frac{\left(\mathrm{R}_{\mathrm{s}}-\mathrm{R}_{\text {bal }}\right)}{2\left(\mathrm{R}_{\mathrm{s}}+\mathrm{R}_{\mathrm{bal}}\right)}
\end{aligned}
$$

## Unbalanced Bridge Analysis

Equation below relates the output voltage change (per volt of supply V ) to the change in sensor resistance.

Original Bridge $\quad \frac{\mathrm{V}_{\mathrm{b}}-\mathrm{V}_{\mathrm{a}}}{\mathrm{V}_{\mathrm{dc}}}=\frac{\left(\mathrm{R}_{\mathrm{s}}-\mathrm{R}_{\mathrm{bal}}\right)}{2\left(\mathrm{R}_{\mathrm{s}}+\mathrm{R}_{\mathrm{bal}}\right)} \quad$ When $\mathrm{R}_{3}=\mathrm{R}_{4}$


## Bridge Output Linearity Analysis

Example: An unbalanced bridge circuit converts temperature sensor resistance into a differential voltage that is amplified by a instrumentation amplifier. The temperature sensor has a resistance of 120 ohms at 35 C and a resistance range of go to 150 ohms.
1.) Design a dc bridge circuit with a 10 V supply that will give zero output at 35 C .
a.) Using $R_{3}=R_{4}=1000$ ohms
b.) Using $R_{3}=120, R_{4}=1000$ ohms
2.) Plot the output voltage over the range of operation at 5 ohm increments for both designs a.) $R_{3}=R_{4}=1000$ ohms b.) $R_{3}=120$ and $R_{4}=1000$ ohms
3.) Find the zero based linear approximation of the bridge output responses.
4.) Determine the maximum non-linearity for each case
5.) Determine the gain required for the instrumentation amplifier gain if a span of 15 V dc is required.

## Bridge Output Linearity Analysis

Example Solution (Part 1a) Balance bridge with $R_{3}=R_{4}=1000$ ohms


Example Solution (Part 1b) Balance bridge with $R_{3}=120$ ohms $R_{4}=1000$ ohms

$$
\begin{array}{ll}
\frac{R_{s}}{R_{2}}=\frac{R_{3}}{R_{4}} \quad \frac{120}{R_{2}}=\frac{120}{1000} \\
R_{2}=1000
\end{array}
$$

## Bridge Output Linearity Analysis

Example Solution (Part 2a) plot output $V$ with $R_{3}=R_{4}=1000$ ohms

$$
\begin{aligned}
& V_{b}-V_{a}=\frac{\left(R_{s}-R_{b a l}\right)}{2\left(R_{s}+R_{b a l}\right)} V_{d c} \\
& R_{\text {bal }}=\frac{R_{2} R_{4}}{R_{3}}=\frac{120(1000)}{1000}=120 \quad R_{b a l}=120
\end{aligned}
$$

Plot values of $R_{s}$ from 90 to 150 with Excel or MathCAD using the equation below

$$
\mathrm{V}_{\mathrm{d}}=\mathrm{V}_{\mathrm{b}}-\mathrm{V}_{\mathrm{a}}=\frac{\left(\mathrm{R}_{\mathrm{s}}-120\right)}{2\left(\mathrm{R}_{\mathrm{s}}+120\right)} 10
$$

Sample calculation
$R_{s}=900 h m s$

$$
\begin{aligned}
& \mathrm{V}_{\mathrm{d}}=\left[\frac{(90 \Omega-120 \Omega)}{2 \cdot(90 \Omega+120 \Omega)}\right] \cdot 10 \cdot \mathrm{~V} \\
& \mathrm{~V}_{\mathrm{d}}=-0.714 \mathrm{~V}
\end{aligned}
$$

## Output Plot $R_{3}=R_{4}=1000$ Ohms

| $\mathrm{r}_{\mathrm{S}}=$ | $\mathrm{V}_{\mathrm{d}}\left(\mathrm{r}_{\mathrm{s}}\right)$ |
| :---: | :---: |
| 90 | -0.714 |
| 95 | -0.581 |
| 100 | -0.455 |
| 105 | -0.333 |
| 110 | -0.217 |
| 115 | -0.106 |
| 120 | 0 |
| 125 | 0.102 |
| 130 | 0.2 |
| 135 | 0.294 |
| 140 | 0.385 |
| 145 | 0.472 |
| 150 | 0.556 |



Non-linear output

## Linearity With R3 Not Equal to R4

Example Solution (Part 2b) plot output V with $\mathrm{R}_{3}=120 \mathrm{R}_{4}=1000$ ohms
Use the alternative formula written as function of $r_{s \prime}$, sensor resistance

$$
\mathrm{V}_{\mathrm{d} 1}\left(\mathrm{r}_{\mathrm{s}}\right)=\left[\frac{\mathrm{R}_{4} \cdot\left(\mathrm{r}_{\mathrm{s}}-\mathrm{R}_{\mathrm{bal}}\right)}{\left(\mathrm{R}_{3}+\mathrm{R}_{4}\right) \cdot\left(\mathrm{r}_{\mathrm{s}}+\frac{\mathrm{R}_{\mathrm{bal}} \cdot \mathrm{R}_{4}}{\mathrm{R}_{3}}\right)}\right] \cdot \mathrm{V}_{\mathrm{dc}}
$$

Where

$$
\mathrm{R}_{\text {bal }}=\frac{\mathrm{R}_{2} \cdot \mathrm{R}_{3}}{\mathrm{R}_{4}}=\frac{(1000 \Omega)(120 \Omega)}{1000 \Omega}=120 \Omega
$$

Substitute
Values

$$
\begin{aligned}
\mathrm{V}_{\mathrm{d}}\left(\mathrm{r}_{\mathrm{s}}\right):=\frac{(1000 \Omega) \cdot\left(\mathrm{r}_{\mathrm{s}}-120 \Omega\right) \cdot 10 \cdot \mathrm{~V}}{(1120 \Omega) \cdot\left(\mathrm{r}_{\mathrm{s}}+1000 \Omega\right)} & \mathrm{V}_{\mathrm{d} 1}=\frac{(1000 \Omega)}{(1120 \Omega} \\
\text { Sample Calculation } & \mathrm{V}_{\mathrm{d} 1}=-0.246 \mathrm{~V}
\end{aligned}
$$

## Output Plot $R_{3}=120$ and $R_{4}=1000$ Ohms

| $\mathrm{V}_{\mathrm{d} 1}\left(\mathrm{r}_{\mathrm{s}}\right)$ | $\mathrm{r}_{\mathrm{S}}=$ |
| :---: | :---: |
| -0.246 | 90 |
| -0.204 | 95 |
| -0.162 | 100 |
| -0.121 | 105 |
| -0.08 | 110 |
| -0.04 | 115 |
| 0 | 120 |
| 0.04 | 125 |
| 0.079 | 130 |
| 0.118 | 135 |
| 0.157 | 140 |
| 0.195 | 145 |
| 0.233 | 150 |



Less output voltage than first case

## Linear Approximations

Example Solution (Part 3) Find zero based linear approximation. Assume line passes through zero and the average of the end points

For bridge with $\mathrm{R}_{3}=\mathrm{R}_{4}=1000$ ohms

$$
\begin{aligned}
& \text { at } R_{s}=90 \quad V_{d}=-0.714 \\
& \text { at } R_{s}=150 \quad V_{d}=0.556
\end{aligned}
$$

Average max value $(|-0.714|+|0.556|) / 2=0.635$
Use two data points:

$$
\begin{aligned}
& R_{\mathrm{s} 1}=120 \quad V_{d_{1}}=0 \\
& R_{\mathrm{s} 2}=150 \quad V_{d 2}=V_{a v e}=0.635
\end{aligned}
$$

Use two-point form of line to find equation

$$
\begin{aligned}
& \left(\mathrm{V}_{\mathrm{d}}-\mathrm{V}_{\mathrm{d} 1}\right)=\frac{\left(\mathrm{V}_{\mathrm{d} 2}-\mathrm{V}_{\mathrm{d} 1}\right)}{\left(\mathrm{R}_{\mathrm{s} 2}-\mathrm{R}_{\mathrm{s} 1}\right)}\left(\mathrm{r}_{\mathrm{s}}-\mathrm{R}_{\mathrm{s} 1}\right) \\
& \left(\mathrm{V}_{\mathrm{d}}-0\right)=\frac{(0.635-0)}{(150-120)}\left(\mathrm{r}_{\mathrm{s}}-120\right) \\
& \mathrm{V}_{\mathrm{d}}=0.021167 \mathrm{r}_{\mathrm{s}}-2.54 \text { Equation }
\end{aligned}
$$

## Linear Approximations

For bridge with $R_{3}=R_{4}=1000 \mathrm{ohms}$

Non-linearity
Increase as
$\mathrm{R}_{\mathrm{s}}$ moves from
balance point


## Linear Approximations

For bridge with $\mathrm{R}_{3}=120, \mathrm{R}_{4}=1000$ ohms

$$
\begin{aligned}
& \text { at } R_{s 1}=90 \quad V_{d 1}=-0.246 \\
& \text { at } R_{s 2}=150 \quad V_{d 2}=0.233
\end{aligned}
$$

Average max value $(|-0.246|+|0.233|) / 2=0.2395$


$$
\begin{aligned}
& \left(V_{d}-V_{d 1}\right)=\frac{\left(V_{d 2}-V_{d 1}\right)}{\left(R_{2}-R_{1}\right)}\left(r_{s}-R_{1}\right) \\
& \left(V_{d}-0\right)=\frac{(0.2395-0)}{(150-120)}\left(r_{s}-120\right) \\
& \quad V_{d}=0.007983 r_{s}-0.958 \text { Equation }
\end{aligned}
$$

Less output voltage but greater linearity Dc bridge approximately linear for small deviations around balance point

## Maximum Non-Linearity

Example Solution (Part 4) Determine the maximum non-linearity for each bridge.
Take difference between actual bridge output and the zero based lines.
Maximum occurs at either end of the graph.


## Percent Non-Linearity

Determine the percent non-linearity using the following formula

\%error $=\frac{\left|\mathrm{V}_{\mathrm{dl}}-\mathrm{V}_{\mathrm{d}}\right|}{\left|2 \cdot \mathrm{~V}_{\mathrm{dl}(\max )}\right|} 100 \%$
Where $\mathrm{V}_{\mathrm{dl}(\text { max })}=$ max linear output
$\cdots \times \mathrm{R} 3=\mathrm{R} 4$
$\mathrm{R} 3=120, \mathrm{R} 4=1000$

## Instrumentation Amplifier Gains

Example Solution (Part 5) Determine the gain necessary for a span of 15 Vdc
Use average value of $\mathrm{V}_{\mathrm{d}}$ to compute gain

For $\mathrm{R}_{3}=\mathrm{R}_{4}=1000$ ohms
Average max value
$(|-0.714|+|0.556|) / 2=0.635 \mathrm{~V}$


For $R_{3}=120$ and $R_{4}=1000$ ohms
Average max value
$(|-0.246|+|0.233|) / 2=0.2395 \mathrm{~V}$

## Instrumentation Amplifier Gains

Compute the Amp gains using the gain formula

For $R_{3}=R_{4}=1000$ ohms
$\mathrm{V}_{0}=15 \mathrm{~V}$ dc $\mathrm{V}_{\mathrm{d}}=0.635 \mathrm{~V}$
$\frac{V_{0}}{V_{d}}=\frac{R_{f}}{R_{a}}=A_{V}$
$\frac{15 \mathrm{~V}}{0.635 \mathrm{~V}}=\frac{\mathrm{R}_{\mathrm{f}}}{\mathrm{R}_{\mathrm{a}}}=\mathrm{A}_{\mathrm{V}}$
$23.62=\mathrm{A}_{\mathrm{v}}$

For R3=120 and R4 $=1000$ ohms

$$
\begin{aligned}
& \mathrm{V}_{0}=15 \mathrm{~V} \text { dc } \mathrm{V}_{\mathrm{d}}=0.2395 \mathrm{~V} \\
& \frac{\mathrm{~V}_{0}}{\mathrm{~V}_{\mathrm{d}}}=\frac{\mathrm{R}_{\mathrm{f}}}{\mathrm{R}_{\mathrm{a}}}=\mathrm{A}_{\mathrm{V}} \\
& \frac{15 \mathrm{~V}}{0.2395 \mathrm{~V}}=\frac{\mathrm{R}_{\mathrm{f}}}{\mathrm{R}_{\mathrm{a}}}=\mathrm{A}_{\mathrm{V}} \\
& 62.63=\mathrm{A}_{\mathrm{V}}
\end{aligned}
$$

Note that increasing linearity reduces $\mathrm{V}_{\mathrm{d}}$ and requires higher gains

## End Lesson 12: Analog Signal Conditioning

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